

Compact Modeling for Open and Short Structures in RF CMOS Technology over 0.25-110 GHz

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1、 Introduction

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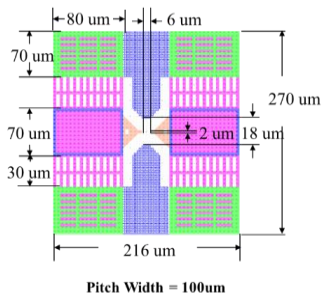
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1、 Introduction

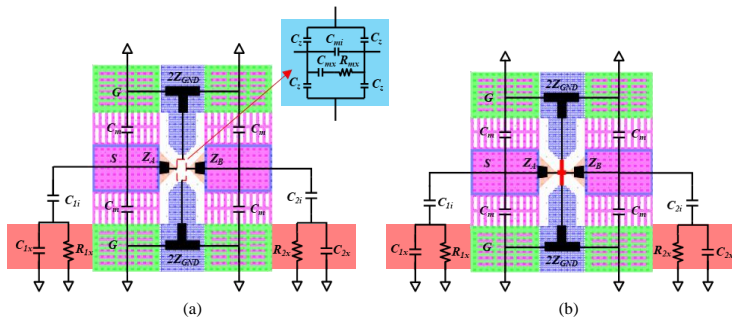
- The operation frequency of the RF-IC manufactured in CMOS technologies have reached well over 100 GHz
- GSG pads are commonly used in most of the integrated circuit design for on-wafer testing.
- A complete and accurate modeling method for open and short test structure with GSG pads are still lack.

2、 Model Development and Extraction



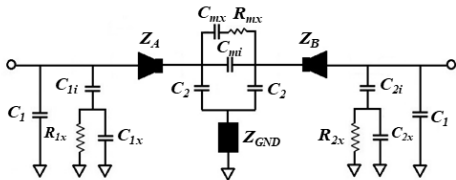
Simplified layout of a GSG pad in RF CMOS technology.

2、 Model Development and Extraction



The proposed equivalent circuit model for open and short structures.

2、 Model Development and Extraction

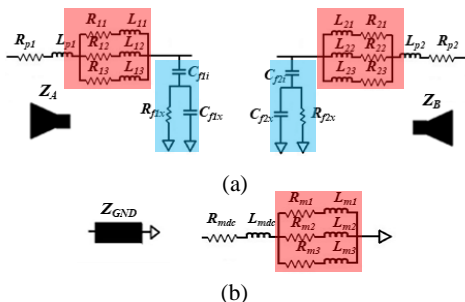


$$C_1 = 2C_m$$

$$C_2 = 2C_z$$

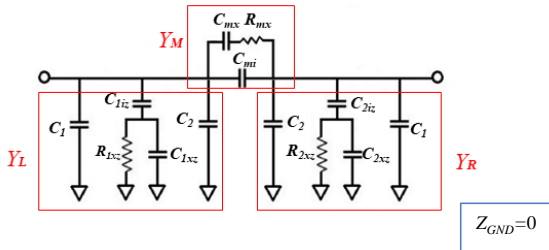
Simplified model topology for the open structure.

2、Model Development and Extraction



- (a) Equivalent circuits for the metal feedlines at port 1 and port 2.
- (b) Equivalent circuit for the metal ground plane.

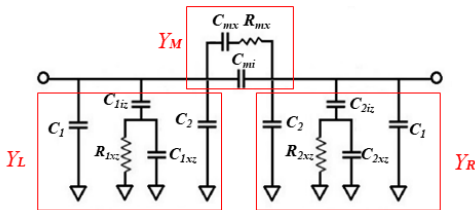
2、 Model Development and Extraction



Simplified model topology for the open test structure at low frequency. The relationships of model elements given as

$$C_{1iz}=C_{f1i} // C_{1i}, C_{1xz}=C_{f1x} // C_{1x} \text{ and } R_{1xz}=R_{f1x} // R_{1x}.$$

2、 Model Development and Extraction



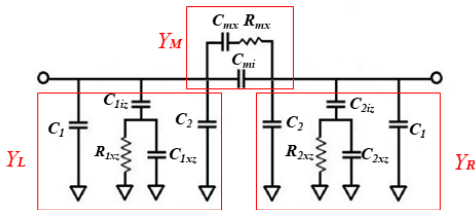
$$Y_M = j\omega C_{mi} + [R_{mx} + (j\omega C_{mx})^{-1}]^{-1}$$

The real and imaginary parts of Y_M can be arranged as follows

$$[\operatorname{Re}(Y_M)]^{-1} = (C_{mx}^2 R_{mx})^{-1} \omega^{-2} + R_{mx}$$

$$\operatorname{Im}(Y_M) = \omega C_{mi} + \omega C_{mx} (1 + \omega^2 C_{mx}^2 R_{mx}^2)^{-1}$$

2、 Model Development and Extraction

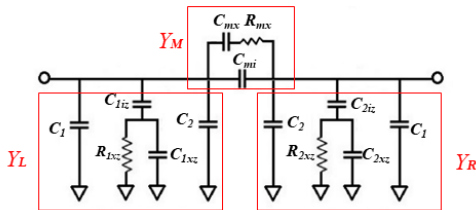


C_{mx} and R_{mx} can be determined from the intercept and slope of $[\text{Re}(Y_M)]^{-1}$ versus ω^{-2} , respectively.

C_{mi} is that can be calculated from as

$$C_{mi} = \text{Im}(Y_M) \omega^{-1} - C_{mx} \left(1 + \omega^2 C_{mx}^2 R_{mx}^2\right)^{-1}$$

2、 Model Development and Extraction



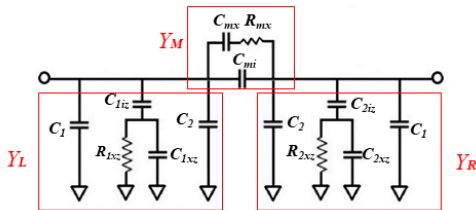
$$Y_L = j\omega(C_1 + C_2) + \left[(j\omega C_{1lx})^{-1} + (j\omega C_{1xz} + R_{1xz}^{-1})^{-1} \right]^{-1}$$

The real and imaginary parts of $[Y_L - j\omega(C_1 + C_2)^{-1}]$ can be arranged as follows

$$\left\{ \text{Re} \left[Y_L - j\omega(C_1 + C_2)^{-1} \right] \right\}^{-1} = R_{1xz}^{-1} + C_{1xz}^2 R_{1xz} \omega^2$$

$$\text{Im} \left[Y_L - j\omega(C_1 + C_2)^{-1} \right]^{-1} = -(\omega C_{1lx})^{-1} - \omega C_{1xz} R_{1xz}^2 (1 + \omega^2 C_{1xz}^2 R_{1xz}^2)^{-1}$$

2、 Model Development and Extraction

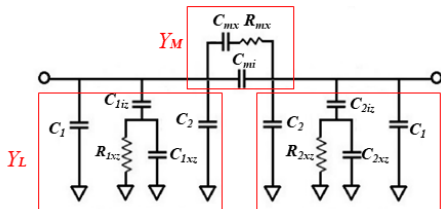


R_{lxz} and C_{lxz} can be determined from the intercept and slope of $\{\text{Re}[Y_L - j\omega(C_1 + C_2)^{-1}]\}^{-1}$ versus ω^2 , respectively.

Once R_{lxz} and C_{lxz} are obtained, C_{lix} can be calculated as

$$C_{lix}^{-1} = -\omega \text{Im}(Y_L - j\omega C_1)^{-1} - \omega^2 C_{lxz} R_{lxz}^2 (1 + \omega^2 C_{lxz}^2 R_{lxz}^2)^{-1}$$

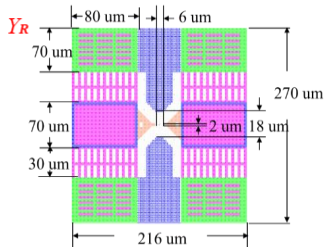
2、 Model Development and Extraction



$$C_{1iz} = C_{f1i} // C_{1i}$$

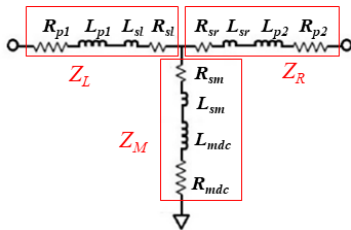
$$C_{1xz} = C_{f1x} // C_{1x}$$

$$R_{1xz} = R_{f1x} // R_{1x}$$



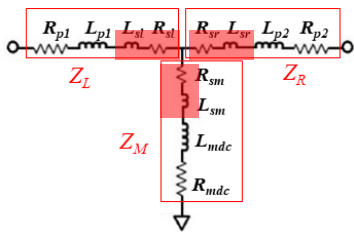
Pitch Width = 100um

2、 Model Development and Extraction



The equivalent circuit of the short structure after open deembedded, e.g. $Y_{\text{short}} - Y_{\text{open}}$. The model topology is low frequency accurate.

2、 Model Development and Extraction



$$Z_L = (R_{p1} + R_{sl}) + j\omega(L_{p1} + L_{sl})$$

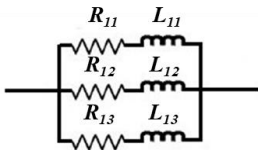
$$Z_R = (R_{p2} + R_{sr}) + j\omega(L_{p2} + L_{sr})$$

$$Z_M = (R_{mdc} + R_{sm}) + j\omega(L_{mdc} + L_{sm})$$

L_{sl} , R_{sl} , L_{sr} , R_{sr} and L_{sm} , R_{sm} are generally small and can be ignored.

R_{p1} , R_{p2} , R_{mdc} and L_{p1} , L_{p2} , L_{mdc} are that determined from the real and imaginary parts of Z_L , Z_R and Z_M as $R_{p1} = \text{Re}(Z_L)$, $R_{p2} = \text{Re}(Z_R)$, $R_{mdc} = \text{Re}(Z_M)$ and $L_{p1} = \text{Imag}(Z_L)/\omega$, $L_{p2} = \text{Imag}(Z_R)/\omega$, $L_{mdc} = \text{Imag}(Z_M)/\omega$, respectively.

2、 Model Development and Extraction



The skin effect elements L_{11} , L_{12} , L_{13} and R_{11} , R_{12} , R_{13} can be determined by using empirical formula.

$$L_{1m} = K_1 \times 10^{-7} \times 2 \times l_{total} \times \left[\ln \left(\frac{2 \times l_{total}}{w_{ms} + h_{1s}} \right) + 0.50049 + \frac{w_{ms} + h_{ms}}{3 \times l_{total}} \right]$$

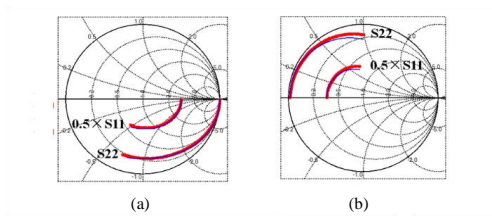
$$R_{1m} = K_2 \times l_{total} / (condtls \times h_{ms} \times w_{ms}) \quad (m=1,2,3)$$

3、 Model Verification

Table 1. Initially Extracted and Optimized Values of the Model Parameters RMS Error = $|\text{Extracted Value} - \text{Optimized Value}| / \text{Extracted Value} \times 100\%$

| Parameter | Extracted | Optimized | Error(%) |
|---|--------------|---------------|-------------|
| $C_{11}/C_{11s}(\times 10^{-15}\text{F})$ | 46.67/90.5 | 44.63/88.5 | 4.4/2.2 |
| $C_{r12}/C_{r12s}(\times 10^{-15}\text{F})$ | 0.83/1.62 | 0.83/1.616 | 0/0.24 |
| $C_{21}/C_{21s}(\times 10^{-15}\text{F})$ | 47.06/96.9 | 45.72/102.7 | 2.8/6 |
| $C_{r22}/C_{r22s}(\times 10^{-15}\text{F})$ | 0.84/1.73 | 0.83/1.7 | 1.2/1.7 |
| $R_{12}/R_{12s}(\Omega)$ | 26.75/27.67 | 25.66/26.54 | 4.1/4.08 |
| $R_{r12}/R_{r12s}(\times 10^3\Omega)$ | 1.498/1.55 | 1.5/1.548 | 0.13/0.13 |
| $L_{22}/L_{22s}(\times 10^{-12}\text{H})$ | 28.5/30 | 27.9/28.2 | 2.1/6 |
| $R_{22}/R_{22s}(\times 10^{-3}\Omega)$ | 192/196 | 189.6/196.9 | 1.3/0.5 |
| $L_{mdc}(\times 10^{-12}\text{H})$ | 1.8 | 1.65 | 8.3 |
| $R_{mdc}(\times 10^{-3}\Omega)$ | 244 | 248.9 | 2 |
| $L_{11}/L_{11s}/L_{113}(\times 10^{-12}\text{H})$ | 4/4.2/5.12 | 3.8/4.3/5.1 | 5/2.4/0.4 |
| $R_{11}/R_{11s}/R_{113}(\Omega)$ | 0.6/0.37/0.3 | 0.6/0.37/0.28 | 0.3/0/1 |
| $L_{22}/L_{22s}/L_{223}(\times 10^{-12}\text{H})$ | 4/4.2/5.12 | 4.1/4.1/5.1 | 2.5/2.4/0.4 |
| $R_{22}/R_{22s}/R_{223}(\Omega)$ | 0.6/0.37/0.3 | 0.6/0.36/0.29 | 0/1.1/0.7 |
| $C_{m1}/C_{m1s}(\times 10^{-15}\text{F})$ | 2/5.0 | 1.97/5.33 | 1.5/6.6 |
| $R_{m1}(\Omega)$ | 344 | 322.6 | 6.2 |
| $C_1(\times 10^{-15}\text{F})$ | 1 | 1.05 | 5 |
| $C_2(\times 10^{-15}\text{F})$ | 4 | 4.1 | 2.5 |
| $L_{m2}/L_{m2s}/L_{m23}(\times 10^{-12}\text{H})$ | 3.4/3.4/4.54 | 3.3/3.3/4.6 | 2.9/2.9/1.3 |
| $R_{m2}/R_{m2s}/R_{m23}(\times 10^{-3}\Omega)$ | 67/34/11 | 67/33/12 | 0/2.9/9 |
| $L_{21}/L_{21s}/L_{21m}(\times 10^{-12}\text{H})$ | 0.5/0.5/0.5 | 0.49/0.48/0.5 | 2/4/8 |
| $R_{21}/R_{21s}/R_{21m}(\times 10^{-3}\Omega)$ | 35/35/35 | 36/35.2/37 | 2.86/0.6/6 |

3、 Model Verification



The measured and simulated S parameters.

- (a) Open results between measured and simulated values.
- (b) Short results between measured and simulated values.

4、 Conclusion

- A new compact model for GSG pad structure in RF CMOS has been presented.
- A novel model parameter extraction method has been proposed.
- The model simulated results show excellent agreement with the measured results, verified the high accuracy of the proposed model.

Thank you!