

# ***Compact Quasi-Static Small-Signal Model for GaN HEMTs***

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# *Goal*

- ◆ Development of a physical-based compact model for GaN HEMT with analytical expressions of the drain current and the small-signal parameters

# *Outline*

- ◆ Introduction
- ◆ Charge control model
- ◆ DC model
- ◆ Charge and capacitance models
- ◆ Results
- ◆ Conclusion

# *Introduction*

- ◆ Since the use of wide band-gap materials for FETs started, GaN based HEMTs have demonstrated to be one of the best devices for high power and high frequency applications
- ◆ Accurate modeling of GaN HEMTs is therefore critical in high power RF circuit design
- ◆ The fact that most physical models are computationally complex and time consuming restricts their application in circuit simulations.
- ◆ A Call for a standard GaN HEMT model has been opened by the Compact Modeling Council

# *Introduction*

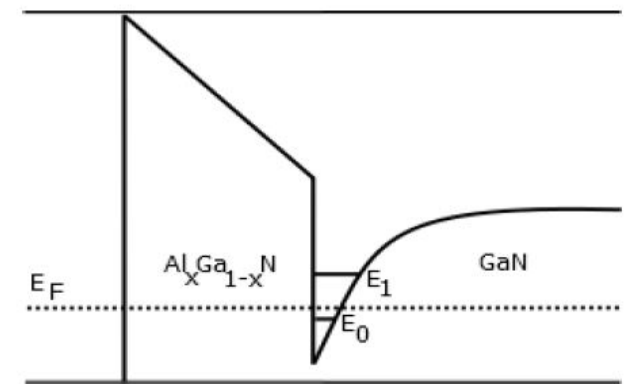
- ◆ We developed a compact and explicit GaN HEMT model based from a charge control model derived from the band structure at the AlGa<sub>N</sub>/Ga<sub>N</sub> interface
- ◆ Analytical expressions, valid for all operating regimes, of the drain current, total charges and small-signal parameters, have been obtained
- ◆ Short-channel effects were included
- ◆ The modeled characteristics agree very well with experimental data

# Charge control model

- ◆ In AlGa<sub>x</sub>N/GaN and AlGaAs/GaAs heterostructures the charge density per unit area accumulated in the potential well at the interface can be calculated with the assumption of a quasi-constant electric field in the potential well (triangular well approximation) and considering that only the contribution of the first subband is important:

$$n_s = DV_{th} \ln \left( \exp \left( \frac{E_f - E_0}{V_{th}} \right) + 1 \right)$$

Where  $E_0 = \gamma_0 n_s^{2/3}$



This results in the following charge control model:

$$V_{g0} = \frac{qdn_s}{\epsilon} + \gamma_0 n_s^{2/3} + V_{th} \ln \left[ \exp \left( \frac{n_s}{DV_{th}} \right) - 1 \right]$$

# Drain current model

- ◆ The drain current expression is obtained from:

$$I_{ds} = W \mu q n_s \frac{dV}{dx}$$

- ◆ Applying the charge control model

$$dV = - \left( \frac{qd}{\epsilon} + \frac{2}{3} \gamma_0 n_s^{-1/3} + V_{th} n_s^{-1} \right) dn_s .$$

- ◆ After integration from source to drain, we obtain:

$$I_{ds} = - \frac{q \mu W}{L} \left[ \frac{qd}{2\epsilon} (n_D^2 - n_S^2) + \frac{2}{5} \gamma_0 (n_D^{5/3} - n_S^{5/3}) + V_{th} (n_D - n_S) \right]$$

# Drain current model

- We use unified and analytical expressions for the charge sheet densities at the source and drain, valid and continuous through all operating regimes

$$n_s = \frac{2V_{th} (C_g / q) \ln(1 + \exp(V_{g0} / 2V_{th}))}{1/H(V_{g0}) + (C_g / qD) \exp(-V_{g0} / 2V_{th})}$$

$$H(V_{go}) = \frac{V_{go} + V_{th} \left[ 1 - \ln(\beta V_{gon}) \right] - \frac{\gamma_0}{3} \left( \frac{C_g V_{go}}{q} \right)^{2/3}}{V_{go} \left( 1 + \frac{V_{th}}{V_{god}} \right) + \frac{2\gamma_0}{3} \left( \frac{C_g V_{go}}{q} \right)^{2/3}}$$



# *Drain current model*

- The main short-channel and second order effects are included in the model.
  - Velocity saturation
  - Channel-length modulation
  - DIBL
  - Self-heating
- To take into account velocity saturation, a saturation voltage is found from a relation between velocity and lateral field. An effective drain-source voltage is used in the model.

# Charge model

- The gate charge expression is derived by integrating the gate charge density and using our unified charge control model

$$Q_G = W \int_0^L qn_s(x) dx.$$

$$Q_G = \frac{W^2 q^2 \mu}{I_{ds}} \int_{V_s}^{V_d} n_s^2 dV$$

- The final expression is:

$$Q_G = WLq \left( \frac{\frac{qd}{3\epsilon} (n_D^3 - n_S^3) + \frac{1}{4} \gamma_0 (n_D^{8/3} - n_S^{8/3}) + \frac{1}{2} V_{th} (n_D^2 - n_S^2)}{\frac{qd}{2\epsilon} (n_D^2 - n_S^2) + \frac{2}{5} \gamma_0 (n_D^{5/3} - n_S^{5/3}) + V_{th} (n_D - n_S)} \right)$$

# Gate capacitance model

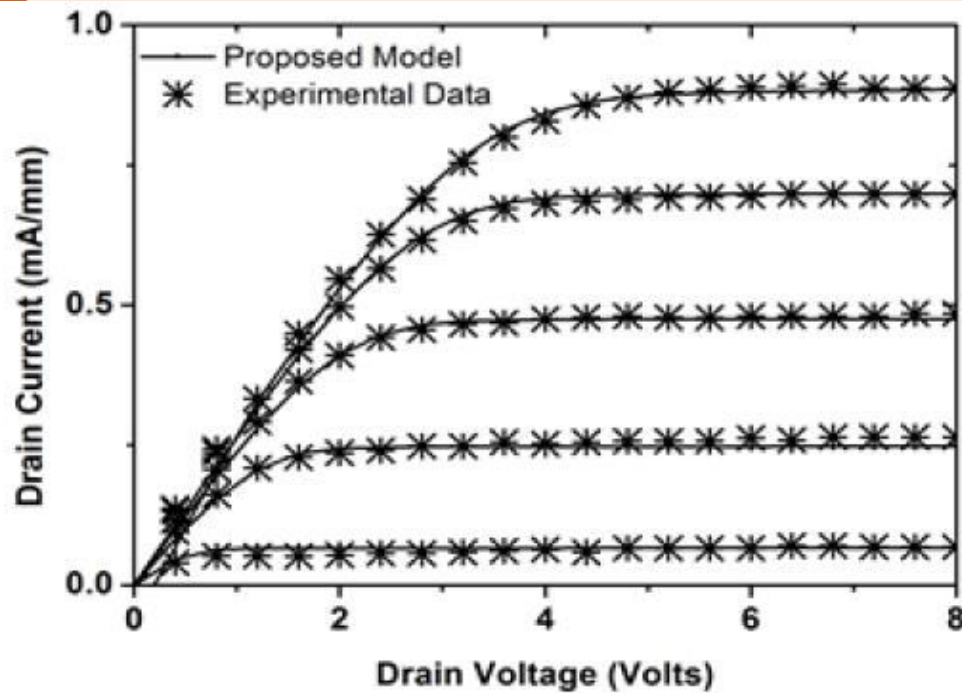
- The gate-source and gate-drain capacitances are obtained by partially differentiating the gate charge with respect to the source and drain voltages

$$C_{Gx} = WLq \left( \frac{\frac{\partial f(n_s)}{\partial V_x} g(n_s) - f(n_s) \frac{\partial g(n_s)}{\partial V_x}}{(g(n_s))^2} \right)$$

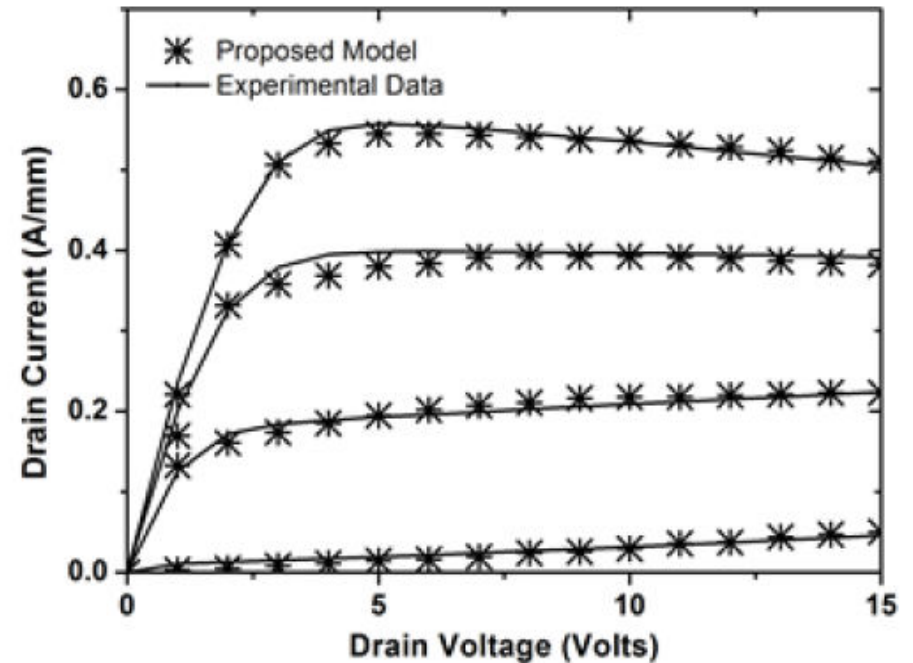
$$f(n_s) = \frac{qd}{3\epsilon} (n_D^3 - n_S^3) + \frac{1}{4} \gamma_0 (n_D^{8/3} - n_S^{8/3}) + \frac{1}{2} V_{th} (n_D^2 - n_S^2)$$

$$g(n_s) = \frac{qd}{2\epsilon} (n_D^2 - n_S^2) + \frac{2}{5} \gamma_0 (n_D^{5/3} - n_S^{5/3}) + V_{th} (n_D - n_S).$$

# Results

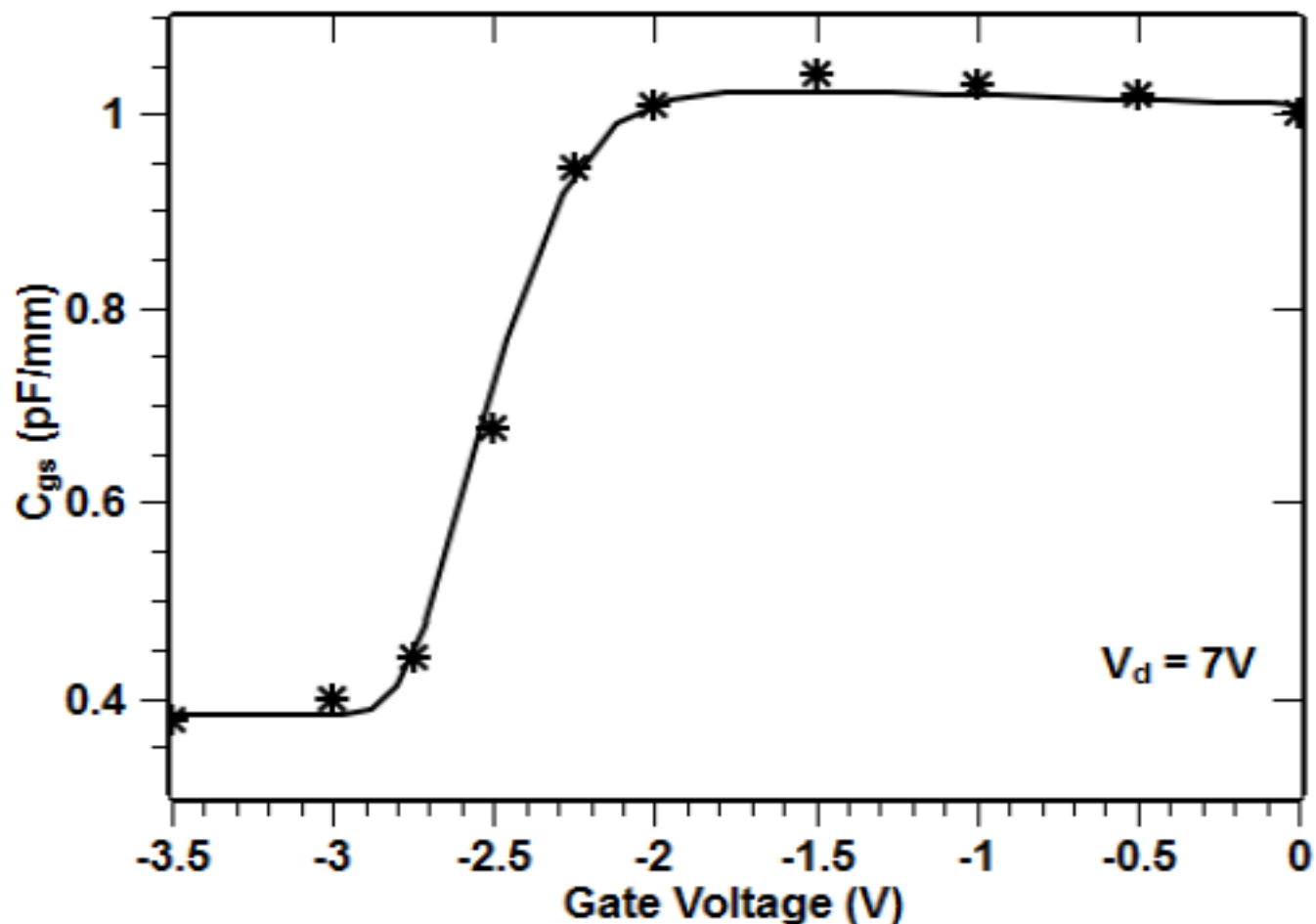


Measured and modeled I-V  
for a GaN HEMT with  $L=0.7 \mu\text{m}$   
 $V_g$  from -3V to 1 V



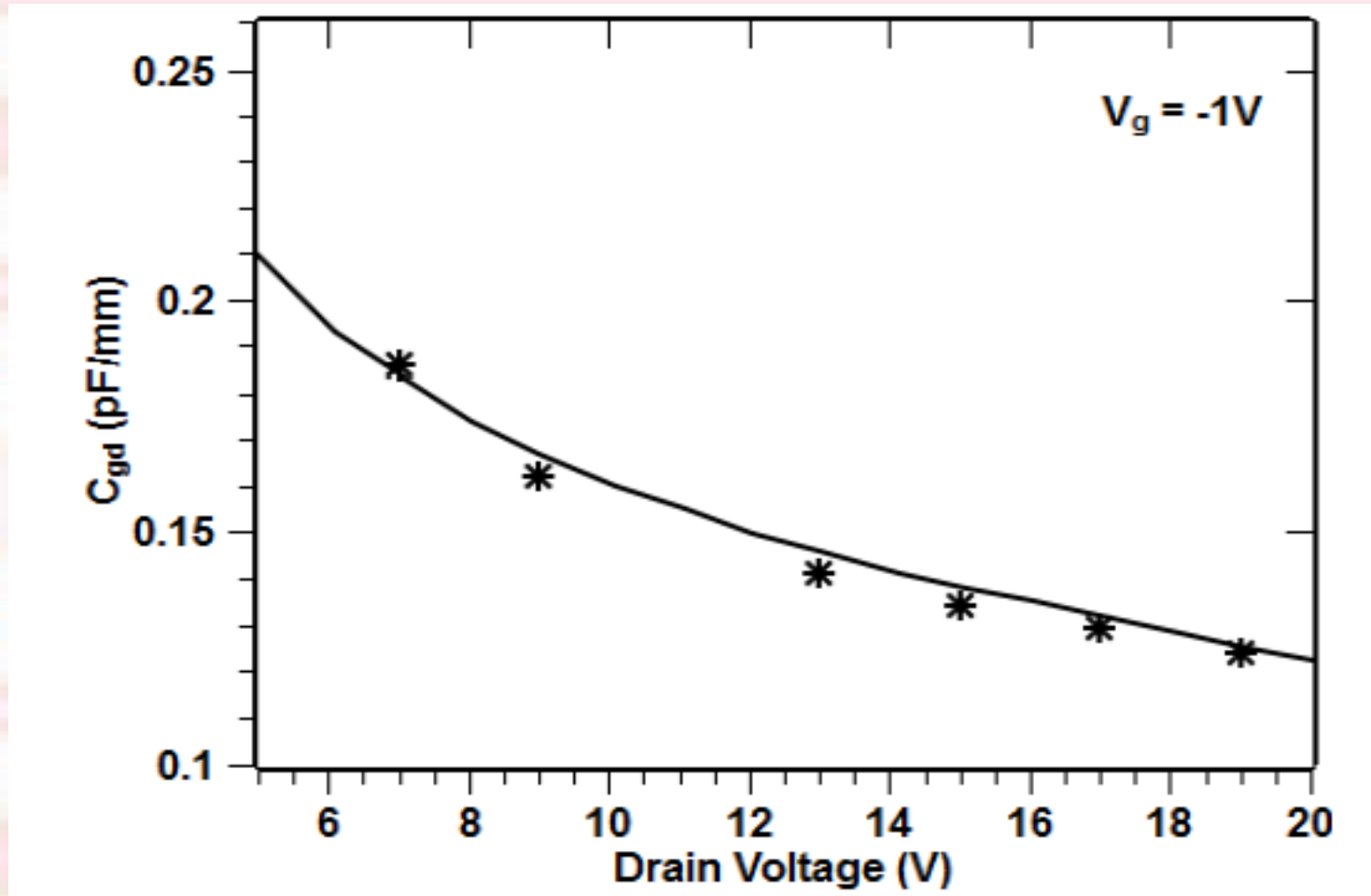
Measured and modeled I-V  
for a GaN HEMT with  $L=0.35 \mu\text{m}$   
 $V_g$  from -3V to 0 V

# Results



Measured and modeled  $C_{gs}$  for a GaN HEMT with  $L=0.35 \mu\text{m}$  at  $V_d = 7V$

# Results



Measured and modeled  $C_{gd}$  for a GaN HEMT with  $L=0.35 \mu\text{m}$  at  $V_g = -1\text{V}$

# *Conclusions*

- We have presented a compact model for AlGaN/GaN with analytical expressions of the small-signal parameters
- The model is developed from a unified charge control model obtained from the band structure of the potential well at the heterointerface considering the contribution of only the first level (assuming a triangular well)
- Good agreement is observed with experimental data

# ***Acknowledgements***

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